

## BSP CASED PILES DATA SHEETS Note No. CP25

### BSP CASED PILES - BASE DRIVING WITH AN INTERNAL DROP HAMMER ESTIMATION OF DRIVING RESISTANCE

The following empirical dynamic formula is based on the results of experience to date:

$$R_u = 290W(1.0 + h)/(S + 12.7)$$

where

$R_u$  = Ultimate driving resistance (tonnes)  
W = Weight of internal drop hammer (tonnes)  
h = ACTUAL drop at final set (metres)  
S = Final set (millimetres per blow)

The formula is APPLICABLE ONLY FOR:

- (i) Drops between 1.2 and 2 metres (vertical piles)
- (ii) Sets less than 5mm per blow (i.e. more than 5 blows per 25mm)

#### NOTES

1. This formula should be used only for piles driven to soils such as sand, gravel, rock, hard marl, or very stiff clay.
2. A re-drive test should be carried out to confirm that the set on re-driving is not greater than at final set on the first drive (See BSP Note No. CP38).
3. The Formula stated above is only applicable where the driving has been carried out exactly in accordance with the recommendations set out in the latest issue of BSP Note No. CP3 'Installation of Casings'.
4. When measuring the final set for application of the formula, it is essential to ensure that the hammer rope is not 'snatched' before the hammer has completed its full drop - otherwise the hammer energy transmitted to the pile is reduced and the formula will give an incorrect and unsafe result.
5. The formula stated above is applicable to vertical piles and in the case of raking piles an appropriate adjustment to the value of the set and/or drop should be made.
6. Owing to the limitations of dynamic pile driving formulae it is generally advisable to test load one or more piles (depending on the size of the contract), particularly when the piles are founded in soils such as stiff clay, chalk, etc.
7. Refer to BSP Note No. CP3 Para. 9 regarding uplifting of piles.
8. Separate checks should be made regarding matters such as the overall stability of the whole group of piles supporting a structure, the possibility of settlement due to a soft stratum existing below the piles, negative friction due to consolidation of an upper soft stratum, and so on. (Refer to Code of Practice 'Foundations' - British Standards Institution.)

## Note No. CP26

The table below is based on the empirical dynamic formula in CP 25 which must be referred to. The details given on this sheet are only applicable under the certain definite conditions stated on CP25.

Dia.	Working Loads (Tonnes)	Hammer W (t)	Drop h (m)	Ultimate Driving Resist. $R_u$ (t)	
				5 Blows/25mm S=5mm	10 Blows/25mm S=2.5mm
254	15-(20)	0.75	1.20	27	31
			1.50	31	36
			1.80	34	40
305	30-(35)	1.25	1.20	45	52
			1.50	51	60
			1.80	57	67
356	40-(50)	2	1.20	72	84
			1.50	82	95
			1.80	92	107
406	50-(60)	2.5	1.20	90	105
			1.50	102	120
			1.80	115	134
457	65-(80)	3	1.20	108	126
			1.50	123	143
			1.80	138	161
508	80-(100)	4	1.20	144	168
			1.50	164	191
			1.80	184	214
559	100-(125)	5	1.20	180	210
			1.50	205	238
			1.80	229	267
610	120-(150)	6	1.20	216	252
			1.50	246	286
			1.80	275	321

#### Notes

1. Figures in brackets (---) are applicable for piles founded in rock, dense sand or gravel, very hard marl or hard shale.
2. Working load is obtained by dividing  $R_u$  (Ultimate Driving Resistance) by Factor of Safety, which is normally 2.

Tex Steel Tubes Ltd (Formerly BSP Limited), Unit 35, Claydon Industrial Park, Gipping Road, Great Blakenham, Ipswich, Suffolk IP6 0JD, England

April 1989